Abstract
Throughout the history of wireless communications, spatial antenna diversity has been important in improving the radio link between wireless users. Historically, microscopic antenna diversity has been used to reduce the fading seen by a radio receiver, whereas macroscopic diversity provides multiple listening posts to ensure that mobile communication links remain intact over a wide geographic area. In recent years, the concepts of spatial diversity have been expanded to build foundations for emerging technologies, such as smart (adaptive) antennas and position location systems. Smart antennas hold great promise for increasing the capacity of wireless communications because they radiate and receive energy only in the intended directions, thereby greatly reducing interference. To properly design, analyze, and implement smart antennas and to exploit spatial processing in emerging wireless systems, accurate radio channel models that incorporate spatial characteristics are necessary. In this tutorial, we review the key concepts in spatial channel modeling and present emerging approaches. We also review the research issues in developing and using spatial channel models for adaptive antennas.

Overview of Spatial Channel Models for Antenna Array Communication Systems

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With the advent of antenna array systems for both interference cancellation and position location applications comes the need to better understand the spatial properties of the wireless communications channel. These spatial properties of the channel will have an enormous impact on the performance of antenna array systems; hence, an understanding of these properties is paramount to effective system design and evaluation.

The challenge facing communications engineers is to develop realistic channel models that can efficiently and accurately predict the performance of a wireless system. It is important to stress here that the level of detail about the environment a channel model must provide is highly dependent on the type of system under consideration. To predict the performance of single-sensor narrowband receivers, it may be acceptable to consider only the received signal power and/or time-varying amplitude (fading) distribution of the channel. However, for emerging wideband multisensor arrays, in addition to signal power level, information regarding the signal multipath delay and angle of arrival (AOA) is needed.

Classical models provide information about signal power level distributions and Doppler shifts of the received signals. These models have their origins in the early days of cellular radio when wideband digital modulation techniques were not readily available. As shown subsequently, many of the emerging spatial models in the literature utilize the fundamental principles of the classical channel models. However, modern spatial channel models build on the classical understanding of fading and Doppler spread, and incorporate additional concepts such as time delay spread, AOA, and adaptive array antenna geometries.

In this article, we review the fundamental channel models that have led to the present-day theories of spatial diversity from both mobile user and base station perspectives. The evolution of these models has paralleled that of cellular systems. Early models only accounted for amplitude and time-varying properties of the channel. These models were then enhanced by adding time delay spread information, which is important when dealing with digital transmission performance. Now, with the introduction of techniques and features that depend on the spatial distribution of the mobiles, spatial information is required in the channel models. As shown in the next sections, more accurate models for the distribution of the scatterers surrounding the mobile and base station are needed. The differentiation between the mobile and base station is important. Classical work has demonstrated that models must account for the physical geometry of scattering objects in the vicinity of the antenna of interest. The number and locations of these scattering objects are dependent on the heights of the antennas, particularly regarding the local environment.

This article, then, explores some of the emerging models for spatial diversity and adaptive antennas, and includes the physical mechanisms and motivations behind the models. A literature survey of existing RF channel measurements with AOA information is also included. The article concludes with a summary and suggestions for future research.

Wireless Multipath Channel Models

This section describes the physical properties of the wireless communication channel that must be modeled. In a wireless system, a signal transmitted into the channel interacts with the environment in a very complex way. There are reflections from large objects, diffraction of the electromagnetic waves
around objects, and signal scattering. The result of these complex interactions is the presence of many signal components, or multipath signals, at the receiver. Another property of wireless channels is the presence of Doppler shift, which is caused by the motion of the receiver, the transmitter, and/or any other objects in the channel. A simplified pictorial of the multipath environment with two mobile stations is shown in Fig. 1. Each signal component experiences a different path environment, which will determine the amplitude $A_{l,k}$, carrier phase shift $\phi_{l,k}$, time delay $\tau_{l,k}$, AOA $\theta_{l,k}$, and Doppler shift $f_d$ of the $l$th signal component of the $k$th mobile. In general, each of these signal parameters will be time-varying.

The early classical models, which were developed for narrowband transmission systems, only provide information about signal amplitude level distributions and Doppler shifts of the received signals. These models have their origins in the early days of cellular radio [14] when wideband digital modulation techniques were not readily available.

As cellular systems became more complex and more accurate models were required, additional concepts, such as time delay spread, were incorporated into the model. Representing the RF channel as a time-variant channel and using a baseband complex envelope representation, the channel impulse response for mobile 1 has classically been represented as [5]

$$h_l(t, t) = \sum_{i=0}^{L(t)-1} A_{i,l}(t) e^{j\phi_{i,l}(t)} \delta(t - \tau_{i,l}(t))$$

where $L(t)$ is the number of multipath components and the other variables have already been defined. The amplitude $A_{l,k}$ of the multipath components is usually modeled as a Rayleigh distributed random variable, while the phase shift $\phi_{l,k}$ is uniformly distributed.

The time-varying nature of a wireless channel is caused by the motion of objects in the channel. A measure of the time rate of change of the channel is the Doppler power spectrum, introduced by M. J. Gans in 1972 [2]. The Doppler power spectrum provides statistical information on the variation of the frequency of a tone received by a mobile traveling at speed $v$. Based on the flat fading channel model developed by R. H. Clarke in 1968, Gans assumed that the received signal at the mobile station came from all directions and was uniformly distributed. Under these assumptions and for a $\lambda/4$ vertical antenna, the Doppler power spectrum is given by [5]

$$S(f) = \begin{cases} \frac{1.5}{\pi f_m} & |f - f_c| < f_m \\ \frac{1}{1 - \left(\frac{f - f_c}{f_m}\right)^2} & |f - f_c| < f_m \\ 0 & \text{elsewhere} \end{cases}$$

where $f_m$ is the maximum Doppler shift given by $v/\lambda$, where $\lambda$ is the wavelength of the transmitted signal at frequency $f_c$.

Figure 2 shows the received signals at the base station, assuming that mobiles 1 and 2 have transmitted narrow pulses at the same time. Also shown is the output of an antenna array system adapted to mobile 1.

The channel model in Eq. 1 does not consider the AOA of each multipath component shown in Figs. 1 and 2. For narrowband signals, the AOA may be included into the vector channel impulse response using

$$h_l(t, t) = \sum_{i=0}^{L(t)-1} A_{i,l}(t) e^{j\phi_{i,l}(t)} d(\theta_{i}(t)) \delta(t - \tau_{i}(t))$$

where $d(\theta(t))$ is the array response vector. The array response vector is a function of the array geometry and AOA. Figure 3 shows the case for an arbitrary array geometry when the array and signal are restricted to two-dimensional space. The resulting array response vector is given by

$$d(\theta(t)) = \begin{bmatrix} \exp(-j\psi_{l,1}) \\ \exp(-j\psi_{l,2}) \\ \vdots \\ \exp(-j\psi_{l,m}) \end{bmatrix}$$

where $\psi_{l}(t) = \frac{\lambda}{2} \left[ x(t) \cos(\theta(t)) + y(t) \sin(\theta(t)) \right] \beta$ and $\beta = 2\pi/\lambda$ is the wavenumber.

The spatial channel impulse response given in Eq. 2 is a summation of several multipath components, each of which has its own amplitude, phase, and AOA. The distribution of these parameters is dependent on the type of environment. In particular, the angle spread of the channel is known to be a function of both the environment and the base station antenna heights. In the next section, we describe macrocell and microcell environments and discuss how the environment affects the signal parameters.

**Macrocell vs. Microcell**

*Macrocell Environment* – Figure 4 shows the channel on the forward link for a macrocell environment. It is usually assumed that the scatterers surrounding the mobile station are about the same height as or are higher than the mobile. This implies that the received signal at the mobile antenna arrives from all directions after bouncing from the surrounding scatterers as illustrated in Fig. 4.

Under these conditions, Gans' assumption that the AOA is uniformly distributed over $[0, 2\pi]$ is valid. The classical
Rayleigh fading envelope with deep fades approximately $\lambda/2$ apart emanates from this model [5].

However, the AOA of the received signal at the base station is quite different. In a macrocell environment, typically, the base station is deployed higher than the surrounding scatterers. Hence, the received signals at the base station result from the scattering process in the vicinity of the mobile station, as shown in Fig. 5. The multipath components at the base station are restricted to a smaller angular region, $\theta_{\text{BP}}$, and the distribution of the AOA is no longer uniform over $[0, 2\pi]$. Other AOA distributions are considered later in this article.

The base station model of Fig. 5 was used to develop the theory and practice of base station diversity in today's cellular system and has led to rules of thumb for the spacing of diversity antennas on cellular towers [3].

**Space: The Final Frontier**

**Details of the Spatial Channel Models**

In the past when the distribution of angle of arrival of multipath signals was unknown, researchers assumed uniform distribution over $[0, 2\pi]$ [7]. In this section, a number of more realistic spatial channel models are introduced. The defining equations (or geometry) and the key results for the models...
are described. Also provided is an extensive list of references.

Table 1 lists some representative active research groups in the field and their Web site addresses where more information on the subject can be found. (Note that this is by no means an exhaustive list.)

The Gaussian Wide Sense Stationary Uncorrelated Scattering (GWSSUS), Gaussian Angle of Arrival (GAA), Typical Urban (TU), and Bad Urban (BU) models described below were developed in a series of papers at the Royal Institute of Technology and may be downloaded from the Web site. Further details of the Geometrically Based Single Bounce (GBSB) models are given in theses at Virginia Tech, which are available at http://etd.vt.edu/etd/index.html.

These various models were developed and used for different applications. Some of the models were intended to provide information about only a single channel characteristic, such as angle spread, while others attempt to capture all the properties of the wireless channel. In the discussion of the models, an effort is made to identify the original motivation of the model and to convey the information the model is intended to provide.

Lee’s Model

In Lee’s model, scatterers are evenly spaced on a circular ring about the mobile as shown in Fig. 6. Each of the scatterers is intended to represent the effect of many scatterers within the region, and hence are referred to as effective scatterers. The model was originally used to predict the correlation between the signals received by two sensors as a function of element spacing. However, since the correlation matrix of the received signal vector of an antenna array can be determined by considering the correlation between each pair of elements, the model has application to any arbitrary array size.

The level of correlation will determine the performance of spatial diversity methods [3, 9]. In general, larger angle spreads and element spacings result in lower correlations, which provide an increased diversity gain. Measurements of the correlation observed at both the base station and the mobile are consistent with a narrow angle spread at the base station and a large angle spread at the mobile. Correlation measurements made at the base station indicate that the typical radius of scatterers is from 100 to 200 wavelengths [3].

Assuming that N scatterers are uniformly placed on the circle with radius R and oriented such that a scatterer is located on the line of sight, the discrete AOAs are [9]

\[ \theta_i = \frac{R}{D} \left( \frac{2\pi i}{N} \right) \quad \text{for } i = 0, 1, \ldots, N - 1. \]

From the discrete AOAs, the correlation of the signals between any two elements of the array can be found using [9]

\[ \rho(d, \theta_0, R, D) = \frac{1}{N} \sum_{i=0}^{N-1} \exp \left( -j 2\pi d \cos(\theta_0 + \theta_i) \right), \]

where \( d \) is the element spacing and \( \theta_0 \) is measured with respect to the line between the two elements as shown in Fig. 6.

The original model provided information regarding only signal correlations. Motivated by the need to consider small-scale fading in diversity systems, Stapleton et al. proposed an extension to Lee’s model that accounts for Doppler shift by imposing an angular velocity on the ring of scatterers [10, 11].

For the model to give the appropriate maximum Doppler shift, the angular velocity of the scatterers within the region, and hence are referred to as effective scatterers. The model was originally used to predict the correlation between the signals received by two sensors as a function of element spacing. However, since the correlation matrix of the received signal vector of an antenna array can be determined by considering the correlation between each pair of elements, the model has application to any arbitrary array size.

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For the model to give the appropriate maximum Doppler shift, the angular velocity of the scatterers must equal \( \nu/R \) where \( \nu \) is the vehicle velocity and \( R \) is the radius of the scatterer ring [11]. Using this model to simulate a Rayleigh fading spatial channel model, the BER for a π/4 differential quadrature phase shift keyed (DQPSK) signal was simulated. The results were compared with measurements taken in a typical suburban environment. The resulting BER estimates were within a factor of two of the actual measured BER, indicating a reasonable degree of accuracy for the model [10].

When the model is used to provide

<table>
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<tr>
<th>Research group</th>
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<tr>
<td>Center for Communications Research — University of Bristol</td>
<td><a href="http://www.fen.bris.ac.uk/elec/research/ccr/ccr.html">http://www.fen.bris.ac.uk/elec/research/ccr/ccr.html</a></td>
</tr>
<tr>
<td>Center for Personkommunikation — Aalborg University</td>
<td><a href="http://www.kom.auc.dk/CPK/">http://www.kom.auc.dk/CPK/</a></td>
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<tr>
<td>Center for Wireless Telecommunications — Virginia Tech</td>
<td><a href="http://www.cwt.vt.edu/">http://www.cwt.vt.edu/</a></td>
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<tr>
<td>Research Group for RF Communications — University of Kaiserlautern</td>
<td><a href="http://www.a-technik.uni-kl.de">http://www.a-technik.uni-kl.de</a></td>
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<tr>
<td>Royal Institute of Technology</td>
<td><a href="http://www.s3.kth.se">http://www.s3.kth.se</a></td>
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<tr>
<td>Smart Antenna Research Group — Stanford University</td>
<td><a href="http://www-isl.stanford.edu/groups/SARG">http://www-isl.stanford.edu/groups/SARG</a></td>
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<tr>
<td>Telecommunications and Information Systems Engineering — University of Texas at Austin</td>
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</tr>
<tr>
<td>Wireless Technology Group — McMaster University</td>
<td><a href="http://www.crl.mcmaster.ca">http://www.crl.mcmaster.ca</a></td>
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Table 1. Some active research groups in the field of adaptive antenna arrays.
Joint AOA and time of arrival (TOA) channel information, one finds that the resulting power delay profile is "U-shaped" [12]. By considering the intersections of the effective scatterers by ellipses of constant delay, one finds that there is a high concentration of scatterers in ellipses with minimum delay, a high concentration of scatterers in ellipses with maximum delay, and a lower concentration of scatterers between. Higher concentrations of scatterers with a given delay correspond with larger powers, and hence larger values on the power delay profile. The "U-shaped" power delay profile is not consistent with measurements. Therefore, an extension to Lee's model is proposed in [11] in which additional scatterer rings are added to provide different power delay profiles.

While the model is quite useful in predicting the correlation between any two elements of the array, and hence the array correlation matrix, it is not well suited for simulations requiring a complete model of the wireless channel.

Discrete Uniform Distribution
A model similar to Lee's model in terms of both motivation and analysis was proposed in [9]. The model (referred to here as the discrete uniform distribution) evenly spaces $N$ scatterers within a narrow beamwidth centered about the line of sight to the mobile as shown in Fig. 7. The discrete possible AOs, assuming $N$ is odd, are given by [9]
\[
\theta_i = \frac{1}{N-1} \theta_{BW}, \quad i = \frac{N-1}{2}, \ldots, \frac{N-1}{2}.
\]

From this, the correlation of the signals present at two antenna elements with a separation of $d$ is found to be
\[
\rho(d, \theta_0, \theta_{BW}) = \frac{1}{N} \sum_{i=-\frac{N-1}{2}}^{\frac{N-1}{2}} \exp[-j2\pi d \cos(\theta_0 + \theta_i)].
\]

Measurements reported in [9] suggest that the AOA statistics in rural and suburban environments are Gaussian distributed (see the discussion of the GAA model later). However, in practice the AOA will be discrete (i.e., a finite number of samples from a Gaussian distribution), and therefore it is not valid to use a continuous AOA distribution to estimate the correlation present between different antenna elements in the array. The correlation that results from a continuous AOA distribution decreases monotonically with element spacing, whereas the correlation that results from a discrete AOA has damped oscillations present. Therefore, a continuous AOA distribution will underestimate the correlation that exists between the elements in the array [9].

In [9], a comparison is made between the correlation obtained using the discrete uniform distribution model, Lee's model, and a continuous Gaussian AOA as a function of element spacing. The comparisons indicate that, for small element separations (two wavelengths), the three models have nearly identical correlations. For larger element separations (greater than two wavelengths), the correlation values using the continuous Gaussian AOA are close to zero, while the two discrete models have oscillation peaks with correlations as high as 0.2 even beyond four wavelengths. Additionally, it was found that the correlation of the discrete uniform distribution falls off more quickly than the correlation in Lee's model.

Again, while the model is useful for predicting the correlation between any pair of elements in the array (which can be used to calculate the array correlation matrix), it fails to include all the phenomena, such as delay spread and Doppler spread, required for certain types of simulations.

Geometrically Based Single-Bounce Statistical Channel Models
Geometrically Based Single-Bounce (GBSB) Statistical Channel Models are defined by a spatial scatterer density function. These models are useful for both simulation and analysis purposes. Use of the models for simulation involves randomly placing scatterers in the scatterer region according to the form

![Figure 7. Discrete uniform geometry.](image)

![Figure 8. Circular scatterer density geometry.](image)

![Figure 9. Joint TOA and AOA probability density function at the base station, circular model (log-scale).](image)

![Figure 10. Joint TOA and AOA probability density function at the mobile, circular model (log-scale).](image)
of the spatial scatterer density function. From the location of each of the scatterers, the AOA, TOA, and signal amplitude are determined.

From the spatial scatterer density function, it is possible to derive the joint and marginal TOA and AOA probability density functions. Knowledge of these statistics can be used to predict the performance of an adaptive array. Furthermore, knowledge of the underlying structure of the resulting array response vector may be exploited by beamforming and position location algorithms.

The shape and size of the spatial scatterer density function required to provide an accurate model of the channel is subject to debate. Validation of these models through extensive measurements remains an active area of research.

**Geometrically Based Circular Model (Macrocell Model)**

The geometry of the Geometrically Based Single Bounce Circular Model (GBSBCM) is shown in Fig. 8. It assumes that the scatterers lie within radius \( R_m \) about the mobile. Often the requirement that \( R_m < D \) is imposed. The model is based on the assumption that in macrocell environments where antenna heights are relatively large, there will be no signal scattering from locations near the base station. The idea of a circular region of scatterers centered about the mobile was originally proposed by Jakes [13] to derive theoretical results for the correlation observed between two antenna elements. Later, it was used to determine the effects of beamforming on the Doppler spectrum [14, 15] for narrowband signals. It was shown that the rate and the depth of the envelope fades are significantly reduced when a narrow-beam beamformer is used.

The joint TOA and AOA density function obtained from the model provides some insights into the properties of the model. Using a Jacobian transformation, it is easy to derive the joint TOA and AOA density function at both the base station and the mobile. The resulting joint probability density functions (PDFs) at the base station and the mobile are shown in the box on this page [16].

The joint TOA and AOA PDFs for the GBSBCM are shown in Figs. 9 and 10 for the case of \( D = 1 \) km and \( R_m = 100 \) m from the base station and mobile perspectives, respectively. The circular model predicts a relatively high probability of multipath components with small excess delays along the line of sight. From the base-station perspective, all of the multipath components are restricted to lie within a small range of angles.

The appropriate values for the radius of scatterers can be determined by equating the angle spread predicted by the model (which is a function of \( R_m \)) with measured values. Measurements reported in [9] suggest that typical angle spreads for macrocell environments with a T-R separation of 1 km are approximately two to six degrees. Also, it is stated that the angle spread is inversely proportional to the T-R separation, which leads to a radius of scatterers that ranges from 30 to 200 m [16]. In [3], it is stated that the active scattering region around the mobile is about 100–200 wavelengths for 900 MHz, which provides a range of 30–60 m, roughly the width of wide urban streets.

The GBSBCM can be used to generate random channels for simulation purposes. Generation of samples from the GBSBCM is accomplished by uniformly placing scatterers in the circular scatterer region about the mobile and then calculating the corresponding AOA, TOA, and power levels.

**Geometrically Based Elliptical Model (Microcell Wideband Model)**

The Geometrically Based Single Bounce Elliptical Model (GBSSEM) assumes that scatterers are uniformly distributed within an ellipse, as shown in Fig. 11, where the base station and mobile are the foci of the ellipse. The model was proposed for microcell environments where antenna heights are relatively low, and therefore multipath scattering near the base station is just as likely as multipath scatterering near the mobile [17, 18].

A nice attribute of the elliptical model is the physical interpretation that only multipath signals which arrive with an absolute delay \( \tau \leq \tau_m \) are accounted for by the model. Ignoring components with larger delays is possible since signals with longer delays will experience greater path loss, and hence have relatively low power compared to those with shorter delays. Therefore, provided that \( \tau_m \) is chosen sufficiently large, the model will account for nearly all the power and AOA of the multipath signals.

The parameters \( a_m \) and \( b_m \) are the semimajor axis and semiminor axis values, which are given by

\[
a_m = \frac{c \tau_m}{2},
\]

\[
b_m = \frac{1}{2} \sqrt{c^2 \tau_m^2 - D^2},
\]

where \( \theta_b \) and \( \theta_m \) are the angle of arrival measured relative to the line of sight from the base station and the mobile, respectively.
where $c$ is the speed of light and $\tau_m$ is the maximum TOA to be considered. To gain some insight into the properties of this model, consider the resulting joint TOA and AOA density function. Using a transformation of variables of the original uniform scatterer spatial density function, it can be shown that the joint TOA and AOA density function observed at the base station is given by [16]

$$f_{\tau, \theta_b}(\tau, \theta_b) = \begin{cases} \left( \frac{D^2 - \tau^2}{2\sigma_b^2}\right) \left( \frac{D^2 - \tau^2 - 2\tau \cos \theta_b}{4\sigma_b^2} \right) & \tau \leq \tau_m \\ 0 & \text{elsewhere} \end{cases}$$

where $\theta_b$ is AOA observed at the base station. A plot of the joint TOA and AOA PDF is shown in Fig. 12 for the case of $D = 1$ km and $\tau_m = 5$ $\mu$s. From the plot of the joint TOA and AOA PDF, it is apparent that the GBSBEM results in a high probability of scatterers with minimum excess delay along the line of sight.

The choice of $\tau_m$ will determine both the delay spread and angle spread of the channel. Methods for selecting an appropriate value of $\tau_m$ are given in [18]. Table 2 summarizes the techniques for selecting $\tau_m$ where $E_r$ is the reflection loss in dB, $n$ is the path loss exponent, and $\tau_0$ is the minimum path delay.

To generate multipath profiles using the GBSBEM, the most efficient method is to uniformly place scatterers in the ellipse and then calculate the corresponding AOA, TOA, and power levels from the coordinates of the scatterer. Uniformly placing scatterers in an ellipse may be accomplished by first uniformly placing the scatterers in a unit circle and then calculating the corresponding AOA, TOA, and power levels from the coordinates of the scatterer. By including multiple clusters, frequency-selective fading channels can be modeled using the

**Gaussian Wide Sense Stationary Uncorrelated Scattering**

The GWSSUS is a statistical channel model that makes assumptions about the form of the received signal vector [19–22]. The primary motivation of the model is to provide a general equation for the received signal correlation matrix. In the GWSSUS model, scatterers are assumed to be Gaussian angle correlated. The GWSSUS model assumes that the location and delay associated with each cluster remains constant over several data bursts, $b$. The form of the received signal vector is

$$x_b(t) = \sum_{k=1}^{d} v_{k,b} e^{j[\theta_b(t - \tau_k) - \theta_k]}$$

where $v_{k,b}$ is the superposition of the steering vectors during the $b$th data burst within the $k$th cluster, which may be expressed as

$$v_{k,b} = \sum_{i=1}^{N_k} \alpha_k e^{j\theta_{i,k}} a(\theta_{i,k} - \theta_k),$$

where $N_k$ denotes the number of scatterers in the $k$th cluster, $\alpha_k$ is the amplitude, $\phi_{i,k}$ is the phase, $\theta_k$ is the angle of arrival of the $i$th reflected scatterer of the $k$th cluster, and $a(0)$ is the array response vector in the direction of $0$ [9]. It is assumed that the steering vectors are independent for different $k$.

If $N_k$ is sufficiently large (approximately 10 or more [19]) for each cluster of scatterers, the central limit theorem may be applied to the elements of $v_{k,b}$. Under this condition, the elements of $v_{k,b}$ are Gaussian distributed. Additionally, it is assumed that $v_{k,b}$ is wide sense stationary. The time delays $\tau_k$ are assumed to be constant over several bursts, $b$, whereas the phases $\phi_{i,k}$ change much more rapidly. The vectors $v_{k,b}$ are assumed to be zero mean, complex Gaussian wide sense, stationary random processes where $b$ plays the role of the time argument. The vector $v_{k,b}$ is a multivariate Gaussian distribution, which is described by its mean and covariance matrix. When no line of sight component is present, the mean will be zero due to the random phase $\phi_{i,k}$, which is assumed to be uniformly distributed in the range $0$ to $2\pi$. When a direct path component is present, the mean becomes a scaled version of the corresponding array response vector $E[v_{k,b}] = \alpha(0)$ [9]. The covariance matrix for the $k$th cluster is given by [21]

$$R_k = E[v_{k,b}v_{k,b}^H] = \sum_{i=1}^{N_k} |\alpha_k|^2 E[a(\theta_{0,k} - \theta_{i,k})a^H(\theta_{0,k} - \theta_{i,k})].$$

The model provides a fairly general result for the form of the covariance matrix. However, it does not indicate the number or location of the scattering clusters, and hence requires some additional information for application to typical environments.

**Gaussian Angle of Arrival**

The Gaussian Angle of Arrival (GAA) channel model is a special case of the GWSSUS model described above where only a single cluster is considered ($d = 1$), and the AOA statistics are assumed to be Gaussian distributed about some nominal angle, $\theta_0$, as shown in Fig. 14. Since only a single cluster is considered, the model is a narrowband channel model that is valid when the time spread of the channel is small compared to the inverse of the signal bandwidth; hence, time shifts may be modeled as simple phase shifts [23]. The statistics of the steering vector are distributed as a multivariate Gaussian random variable. Similar to the GWSSUS model, if no line of

<table>
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<th>Criteria</th>
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<td>Fixed maximum delay, $\tau_m$</td>
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<tr>
<td>Fixed threshold $T$ in dB</td>
<td>$\tau_m = 1.07 - 0.32T$</td>
</tr>
<tr>
<td>Fixed delay spread, $\sigma$</td>
<td>$\tau_m = 3.24\sigma + \tau_0$</td>
</tr>
<tr>
<td>Fixed max. excess delay, $\tau_m$</td>
<td>$\tau_m = \tau_i + \tau_0$</td>
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**Table 2. Methods for selection $\tau_m$**
sight is present, then $E\{v_{k,l}\} = 0$; otherwise, the mean is proportional to the array response vector $a(\theta_{\delta})$. For the special case of uniform linear arrays, the covariance matrix may be described by

$$R(\theta_{\delta}, \sigma_{\delta}) = pa(\theta_{\delta})a^H(\theta_{\delta}) \otimes B(\theta_{\delta}, \sigma_{\delta}),$$

where the $(k,l)$ element of $B(\theta_{\delta}, \sigma_{\delta})$ is given by

$$B(\theta_{\delta}, \sigma_{\delta})_{kl} = \exp\left[-2(\pi A(k-l))^2 \sigma_{\delta}^2 \cos^2 \theta\right].$$

$p$ is the receiver signal power, $A$ is the element spacing, and $\otimes$ denotes element-wise multiplication [23].

Time-Varying Vector Channel Model (Raleigh's Model)

Raleigh's time-varying vector channel model was developed to provide both small-scale Rayleigh fading and theoretical spatial correlation properties [24]. The propagation environment considered is densely populated with large dominant reflectors (Fig. 15). It is assumed that at a particular time the channel is characterized by $L$ dominant reflectors. The received signal vector is then modeled as

$$x(t) = \sum_{l=0}^{L(t)-1} a(\theta_{l})L(t)(t) + n(t),$$

where $a$ is the complex path amplitude, $\alpha(t)$ is the modulated signal, and $n(t)$ is additive noise. This is equivalent to the impulse response given in Eq. 2.

The unique feature of the model is in the calculation of the complex amplitude term, $\alpha(t)$, which is expressed as

$$\alpha(t) = \beta_{l}(t) \sqrt{\Gamma_l - \psi(t)},$$

where $\Gamma_l$ accounts for log-normal fading, $\psi(t)$ describes the power delay profile, and $\beta_{l}(t)$ is the complex intensity of the radiation pattern as a function of time. The complex intensity is described by

$$\beta_{l}(t) = K \sum_{n=1}^{N_l} C_n(\theta_{l}) \exp\left\{i \omega_{\delta} \cos(\Omega_{n,l}) \right\},$$

where $N_l$ is the number of signal components contributing to the $l$th dominant reflecting surface, $K$ accounts for the antenna gains and transmit signal power, $C_n(\theta_{l})$ is the complex radiation of the $n$th component of the $l$th dominant reflecting surface in the direction of $\theta_{l}$, $\omega_{\delta}$ is the maximum Doppler shift, and $\Omega_{n,l}$ is the angle toward the $n$th component of the $l$th dominant reflector with respect to the motion of the mobile. The resulting complex intensity, $\beta_{l}(t)$, exhibits a complex Gaussian distribution in all directions away from the mobile [24].

Both the time and spatial correlation properties of the model are compared to theoretical results in [24]. The comparison shows that there is good agreement between the two.

Two Simulation Models (TU and BU)

Next we describe two spatial channel models that have been developed for simulation purposes.

The Typical Urban (TU) model is designed to have time properties similar to the GSM-TU defined in GSM 05.05, while the Bad Urban (BU) model was developed to model environments with large reflectors that are not in the vicinity of the mobile. Although the models are designed for GSM, DCS1800, and PCS1900 formats, extensions to other formats are possible [251].

Both of these models obtain the received signal vector using

$$x(t) = \sum_{n=1}^{N} \sigma_n \exp\left\{-j2\pi f_c \frac{L_\theta(t)}{c} + \beta \left\{1 - \frac{L_\theta(t)}{c} + \Delta \right\} a(\theta_n(t))\right\},$$

where $N$ is the number of scatterers, $f_c$ the carrier frequency, $c$ is the speed of light, $L_\theta(t)$ the path propagation distance, $\beta$ a random phase, and $\Delta$ random delay. In general, the path propagation distance $L_\theta(t)$ will vary continuously with time; hence, Doppler fading occurs naturally in the model.

Typical Urban (TU) – In the TU model, 120 scatterers are randomly placed within a 1 km radius about the mobile [25]. The position of the scatterers is fixed over the duration in which the mobile travels a distance of 5 m. At the end of the 5 m, the scatterers are returned to their original position with respect to the mobile. At each 5 m interval, random phases are assigned to the scatterers as well as randomized shadowing effects, which are modeled as log-normal with distance with a standard deviation of 5–10 dB [25]. The received signal is determined by brute force from the location of each of the scatterers. An exponential path loss law is also applied to account for large-scale fading [21]. Simulations have shown that the TU model and the GSM-TU model have nearly identical power delay profiles, Doppler spectrums, and delay spreads [25]. Furthermore, the AOA statistics are approximately Gaussian and similar to those of the GAA model described above.

Bad Urban (BU) – The BU is identical to the TU model with the addition of a second scatterer cluster with another 120 scatterers offset 45° from the first, as shown in Fig. 16. The scatterers in the second cluster are assigned 5 dB less average power than the original cluster [25]. The presence of the second cluster results in an increased angle spread, which in turn reduces the off-diagonal elements of the array covariance matrix. The presence of the second cluster also causes an increase in the delay spread.

Uniform Sected Distribution

The defining geometry of Uniform Sected Distribution (USD) is shown in Fig. 17 [26]. The model assumes that scatterers are uniformly distributed within an angle distribution of $\theta_{BU}$ and a radial
The magnitude and phase associated with phase \(26\). In \(26\), the model is used to study the effect of angle spread on spatial diversity techniques. A key result is that beam-steering techniques are most suitable for scatter distributions with widths slightly larger than the beamwidths.

**Modified Saleh-Valenzuela's Model**

Saleh and Valenzuela developed a multipath channel model for indoor environment based on the clustering phenomenon observed in experimental data [27]. The clustering phenomenon refers to the observation that multipath components arrive at the antenna in groups. It was found that both the clusters and the rays within a cluster decayed in amplitude with time. The impulse response of this model is given by

\[
h(t) = \sum_{i=0}^{L} \sum_{j=0}^{K_i} \alpha_{ij} \delta(t - T_i - \tau_{ij})
\]

where the sum over \(i\) corresponds to the clusters and the sum over \(j\) represents the rays within a cluster. The variables \(\alpha_{ij}\) are Rayleigh distributed with the mean square value described by a double-exponential decay given by

\[
\alpha_{ij}^{-2} = \alpha_{00}^{-2} \exp(-\tau_{ij}/\Gamma) \exp(\tau_{ij}/\gamma)
\]

where \(\Gamma\) and \(\gamma\) are the cluster and ray time decay constant, respectively. Motivated by the need to include AOA in the channel model, Spencer et al. proposed an extension to the Saleh-Valenzuela's model [28], assuming that the time and the angle are statistically independent, or

\[
h(t,\theta) = h(t) \delta(\theta).
\]

Similar to the time impulse response in Eq. 3, the proposed angular impulse response is given by

\[
h(t) = \sum_{i=0}^{L} \sum_{j=0}^{K_i} \alpha_{ij} \delta(\theta - \Theta_i - \omega_{ij})
\]

where \(\alpha_{ij}\) is the amplitude of the \(j\)th ray in the \(i\)th cluster. The variable \(\Theta_i\) is the mean angle of the \(i\)th cluster and is assumed to be uniformly distributed over \([0, 2\pi]\). The variable \(\omega_{ij}\) corresponds to the ray angle within a cluster and is modeled as a Laplacian distributed random variable with zero mean and standard deviation \(\sigma\):

\[
f(\omega) = \frac{1}{\sqrt{2\sigma}} \exp\left(-\frac{|\omega|}{\sigma}\right).
\]

This model was proposed based on indoor measurements which will be discussed in the fourth section.

**Elliptical Subregions Model (Lu, Lo, and Litva's Model)**

Lu et al. [30] proposed a model of multipath propagation based on the distribution of the scatterers in elliptical subregions, as shown in Fig. 18. Each subregion (shown in a different shade) corresponds to one range of the excess delay time. This approach is similar to the GBS-BEM proposed by Liberti and Rappaport [18] in that an ellipse of scatterers is considered. The primary difference between the two models is in the selection of the number of scatterers and the distribution of those scatterers. In the GBSBEM, the scatterers were uniformly distributed within the entire ellipse. In Lu, Lo, and Litva's model, the ellipse is first subdivided into a number of elliptical subregions. The number of scatterers within each subregion is then selected from a Poisson random variable, the mean of which is chosen to match the measured time delay profile data.

It was also assumed that the multipath components arrive in clusters due to the multiple reflecting points of the scatterers. Thus, assuming that there are \(L\) scatterers with \(K_i\) reflecting points each, the model proposed is represented by

\[
h(t,\theta) = \sum_{i=0}^{L} E_i \theta_i^{(i)}
\]

\[
\times \sum_{k=0}^{K_i} \alpha_{ik} \exp\left(-\left(2\pi f_k t_0 + \gamma_k\right)\right) \delta(t - t_{ik}) E_i \theta_i^{(k)}
\]

where \(\alpha_{ik}\), \(\gamma_k\), and \(t_{ik}\) correspond to the amplitude, time delay, and phase of the signal component from the \(ik\)th reflecting point, respectively. \(f_k\) is the Doppler frequency shift of each individual path, \(\theta_i^{(k)}\) is the angle between the \(ik\)th path and the receiver-to-transmitter direction, and \(\theta_i^{(i)}\) is the amplitude of the \(i\)th scatterer as seen from the transmitter. \(E_i\) is the radiation pattern of the transmit and receive antennas, respectively. The variable \(\theta_i^{(k)}\) was assumed to be Gaussian distributed.

Simulation results using this model were presented in [30], showing that a 60° beamwidth antenna reduces the mean RMS delay spread by about 30–43 percent. These results are consistent with similar measurements made in Toronto using a sectorized antenna [31].

**Extended Tap-Delay-Line Model**

A wideband channel model that is an extension of the traditional statistical tap-delay-line model and includes AOA information was developed by Klein and Mohr [29]. The channel impulse response is represented by

\[
h(t,t_0) = \sum_{w=1}^{W} a_w(t) \delta(t - \tau_w) \delta(\theta - \theta_w).
\]

This model is composed by \(W\) taps, each with an associated time delay \(\tau_w\), complex amplitude \(a_w\), and AOA \(\theta_w\). The joint density functions of the model parameters should be determined from measurements. As shown in [29], measurements can provide histograms of the joint distribution of \(|a|\), \(\tau\), and \(\theta\), and the density functions, which are proportional to these histograms, can be chosen.
Measurement-Based Channel Model

A channel model in which the parameters are based on measurement was proposed by Bianz et al. [32]. The idea behind this approach is to characterize the propagation environment, in terms of scattering points, based on measurement data. The time-variant impulse response takes the form

\[ h(\tau, t) = \int \phi(\tau, \theta) \cdot g(\theta) \cdot f(\tau) \cdot d\theta \]

where \( f(\tau) \) is the impulse response representing the joint transfer characteristic of the transmission system components (modulator, demodulator, filters, etc.), and \( g(\theta) \) is the characteristic of the base station antenna. The term \( \phi(\tau, \theta) \) is the time-variant directional distribution of channel impulse response seen from the base station. This distribution is time-variant due to mobile motion and depends on the location, orientation, and velocity of the mobile station antenna and the topographical and morphographical properties of the propagation area as well. Measurement is used to determine the distribution \( \phi(\tau, \theta) \).

Ray Tracing Models

The models presented so far are based on statistical analysis and measurements, and provide us with the average path loss and delay spread, adjusting some parameters according to the environment (indoor, outdoor, obstructed, etc.). In the past few years, a deterministic model, called ray tracing, has been proposed based on the geometric theory and reflection, diffraction, and scattering models. By using site-specific information, such as building databases or architecture drawings, this technique deterministically models the propagation channel [33–36], including the path loss exponent and the delay spread. However, the high computational burden and lack of detailed terrain and building databases make ray tracing models difficult to use. Although some progress has been made in overcoming the computational burden, the development of an effective and efficient procedure for generating terrain and building data for ray tracing is still necessary.

Channel Model Summary

Table 3 summarizes each of the spatial models presented above.

Spatial Signal Measurements

There have been only a few publications relating to spatial channel measurements. In this section, references are given to these papers, and the key results are described.

In [38], TOA and AOA measurements are presented for outdoor macrocellular environments. The measurements were made using a rotating 9° azimuth beam directional receiver antenna with a 10 MHz bandwidth centered at 1840 MHz. Three environments near Munich were considered, including rural, suburban, and urban areas with base station antenna heights of 12.3 m, 25.8 m, and 37.5 m, respectively. The key observations made include [38]:

- Most of the signal energy is concentrated in a small interval of delay and within a small AOA in rural, suburban, and even many urban environments.
- By using directional antennas, it is possible to reduce the time dispersion.

Another set of TOA and AOA measurements is reported in [39] for urban areas. The measurements were made using a two-element receiver that was mounted on the test vehicle with an elevation of 2.6 m. The transmitting antenna was placed 30 m high on the side of a building. A bandwidth of 10 MHz with a carrier frequency of 2.33 GHz was used. The delay-Doppler spectra observed at the mobile was used to obtain the delay-AOA spectra. The second antenna element is used to remove the ambiguity in AOA that would occur if only the Doppler spectra were known. The results indicate that it is possible to account for most of the major features of the delay-AOA spectra by considering the large buildings in the environment.

Motivated by diversity combining methods, earlier measurements were concerned primarily with determining the correlation between the signals at two antenna elements as a function of the element separation distance. These studies found that, at the mobile, relatively small separation distances were required to obtain a small degree of correlation between the elements, whereas at the base station very large spacing was needed. These findings indicate that there is a relatively small angle spread observed at the base station [6].

Previously, an extension to Saleh-Valenzuela's indoor model, including AOA information, was presented. This extension was proposed based on indoor measurements of delay spread and AOA at 7 GHz made at Brigham Young University [40]. The AOAs were measured using a 60 cm parabolic dish antenna that had a 3 dB beamwidth of 6°. The results showed a clustering pattern in both time and angle domain, which led to the proposed channel model described in [28]. Also, it was observed that the cluster mean angle of arrival was uniformly distributed \([0, 2\pi]\). The distribution of the angle of arrival of the rays within a cluster presented a sharp peak at the mean, leading to the Laplacian distribution modeling. The standard deviation found for this distribution was around 25°. Based on these measurements, a channel model including delay spread and AOA information was proposed, supposing that time and angle were independent variables.

In [41], two-dimensional AOA and delay spread measurement and estimation were presented. The measurements were made in downtown Paris using a channel sounder at 900 MHz and a horizontal rectangular planar array at the receiver. The estimation of AOA, including azimuth and elevation angle, was performed using 2D unitary ESPRIT [42] with a time resolution of 0.1 ms and angle resolution of 5°. The results presented confirmed assumptions made in urban propagation, such as the wave-guiding mechanism of streets and the exponential decay of the power delay profile. Also, it was observed that 90 percent of the received power was contained in the paths with elevation between 0° and 40° with the low elevated paths contributing a larger amount.

Finally, in [43] measurements are used to show the variation in the spatial signature with both time and frequency. Two measures of change are given, the relative angle change given by
<table>
<thead>
<tr>
<th>Model Name</th>
<th>Description</th>
<th>References</th>
</tr>
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<tr>
<td>Lee’s Model</td>
<td>Effective scatterers are evenly spaced on a circular ring about the mobile</td>
<td>[3, 9, 11]</td>
</tr>
<tr>
<td>Discrete Uniform Distribution</td>
<td>Predicts correlation coefficient using a discrete AOA model Extension accounts for Doppler shift</td>
<td>[9]</td>
</tr>
<tr>
<td>Geometrically Based Circular Model (Macrolcell Model)</td>
<td>Assumes that the scatterers lie within circular ring about the mobile AOA, TOA, joint TOA and AOA, Doppler shift, and signal amplitude information is provided Intended for macrocell environments where antenna heights are relatively large</td>
<td>[12–14, 16, 37]</td>
</tr>
<tr>
<td>Geometrically Based Elliptical Model (Microcell Wideband Model)</td>
<td>Scatters are uniformly distributed in an ellipse where the base station and the mobile are the foci of the ellipse AOA, TOA, joint TOA and AOA, Doppler shift, and signal amplitude information is provided Intended for microcell environments where antenna heights are relatively low</td>
<td>[17, 18]</td>
</tr>
<tr>
<td>Gaussian Wide Sense Stationary Uncorrelated Scattering (GWSSUS)</td>
<td>N scatterers are grouped into clusters in space such that the delay differences within each cluster are not resolvable within the transmission signal BW Provides an analytical model for the array covariance matrix</td>
<td>[19–22]</td>
</tr>
<tr>
<td>Gaussian Angle of Arrival (GAA)</td>
<td>Special case of the GWSSUS model with a single cluster and angle of arrival statistics assumed to be Gaussian distributed about some nominal angle Narrowband channel model Provides an analytical model for the array covariance matrix</td>
<td>[23]</td>
</tr>
<tr>
<td>Time-Varying Vector Channel Model (Raleigh’s Model)</td>
<td>Assumes that the signal energy leaving the region of the mobile is Rayleigh faded Angle spread is accounted for by dominant reflectors Provides both Rayleigh fading and theoretical spatial correlation properties</td>
<td>[20]</td>
</tr>
<tr>
<td>Typical Urban</td>
<td>Simulation model for GSM, DCS1800, and PCS1900 Time domain properties are similar to the GSM-TU defined in GSM 05.05 120 scatterers are randomly placed within a 1 km radius about the mobile Received signal is determined by brute force from the location of each of the scatterers and the time-varying location of the mobile AOA statistics are approximately Gaussian</td>
<td>[21, 22, 25]</td>
</tr>
<tr>
<td>Bad Urban</td>
<td>Simulation model for GSM, DCS1800, and PCS1900 Accounts for large reflectors not in the vicinity of the mobile Identical to the TU model with the addition of a second scatterer cluster offset 45° from the first</td>
<td>[21, 22, 25]</td>
</tr>
<tr>
<td>Uniform Sectedor Distribution</td>
<td>Assumes that scatterers are uniformly distributed within an angular distribution of θ_{BW} and a radial range of ΔR centered about the mobile Magnitude and phase associated with each scatterer are selected at random from a uniform distribution of [0, 1] and [0, 2π], respectively</td>
<td>[26]</td>
</tr>
<tr>
<td>Modified Saleh-Valenzuela’s Model</td>
<td>An extension to the Saleh-Valenzuela model, including AOA information in the channel model Assumes that time and the angle are statistically independent Based on indoor measurements</td>
<td>[28]</td>
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<tr>
<td>Extended Tap-Delay-Line Model</td>
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<td>Spatio-Temporal Model (Lu, Lo, and Litva’s Model)</td>
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</tr>
</tbody>
</table>

Table 3. Summary of spatial channel models.
while others are intended primarily for simulation purposes.

The availability of channel models provides different angle spreads and hence will be of use in the analysis and design of systems that utilize adaptive antenna arrays. Some of the models were developed to provide analytical models of the spatial correlation function, while others are intended primarily for simulation purposes.

Algorithm Development

The availability of channel models also opens up the possibility of developing new maximum likelihood smart antennas and AOA estimation algorithms based on these channel models. Good analytical models that will provide insights into the structure of the spatial channel are needed.

Conclusions

As antenna technology advances, radio system engineers are increasingly able to utilize the spatial domain to enhance system performance by rejecting interfering signals and boosting desired signal levels. However, to make effective use of the spatial domain, design engineers need to understand and appropriately model spatial domain characteristics, particularly the distribution of scatterers, angles of arrival, and the Doppler spectrum. These characteristics tend to be dependent on the height of the transmitting and receiving antennas relative to the local environment. For example, the distributions expected in a microcellular environment with relatively low base station antenna heights are usually quite different from those found in traditional macrocellular systems with elevated base station antennas.

This article has provided a review of a number of spatial propagation models. These models can be divided into three groups:

1. General statistically based models
2. More site-specific models based on measurement data
3. Entirely site-specific models

The first group of models (Lee's Model, Discrete Uniform Distribution Model, Geometrically Based Single Bounce Statistical Model, Gaussian Wide Sense Stationary Uncorrelated Scattering Model, Gaussian Angle of Arrival Model, Uniform Sected Distributed Model, Modified Saleh-Valenzuela's Model, Spatio-Temporal Model) are useful for general system performance analysis. The models in the second group (Extended Tap Delay Line Model and Measurement-Based Channel Model) can be expected to yield greater accuracy but require measurement data as an input. An example from the third group of models is Ray Tracing, which has the potential to be extremely accurate but requires a comprehensive description of the physical propagation environment as well as measurements to validate the models.

Further research is required to validate and enhance the models described in this article. Bearing in mind that an objective of modeling is to substantially reduce the amount of physical measurement required in the system planning process, it is important for design engineers to have reliable models of AOA, TDOA, delay spread, and the power of the multipath components. Further measurement programs that focus on spatial domain signal characteristics are required. These programs would greatly benefit from the development of improved measurement equipment.

Armed with improved spatial channel modeling tools and a greater understanding of signal propagation, engineers can begin to meet the challenges inherent in designing future high-capacity/high-quality wireless communication systems, including the effective use of smart antennas.

References


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Additional Reading


Biographies

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